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WHITE PAPER

Multiscale assessment on the quality of metal powder feedstocks for additive manufacturing

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INTRODUCTION

Additive manufacturing (AM) is attractive for producing parts with access to unprecedented geometry/configuration complexity, material composition gradient control, and lightweight structure design not attainable by traditional processes. However, the long-term success of this rapidly developing technology hinges, to a large degree, on the ability to produce functional parts and components reliably. Controlling defects is of primary importance to attain AM metal parts with mechanical strength and fatigue life approaching their forged counterparts. Defects in AM parts fall into two main categories: porosity and crack. These can be incurred by various mechanisms: lack of fusion, keyhole collapse, gas porosity, balling, solidification cracking, solid-state cracking, and surface-connected porosity. Defects can also result from entrapment of impurities.¹ Defects arise from the interplay between feedstock and AM beam energy, which involves complex, transient thermophysical and chemical processes (Scheme 1). As such, defects can be feedstock-, equipment-, and processesrelated.² Consequently, defect reduction starts with the quality

control of feedstocks.

Two mainstream AM technologies, i.e., laser powder bed fusion (PBF) and blown powder direct energy deposition (DED), use spherical powder feedstocks with the desired compositions and particle sizes, typically in the range of 10 to 50 microns. In this kind of matter in particulate form, the population of surface and subsurface atoms represent four to five orders larger ratio as compared to bulk materials. While bulk chemistry still lays the foundation for ultimate mechanical properties, the surface chemistry of micro sized powders is becoming equally important, if not greater, for the quality of finished AM parts. Driven by the increased surface free energy (i.e., thermodynamic favorable) and the decrease in diffusion length (i.e., kinetic favorable), the particle-to-particle uniformity of AM metal powder is inherently susceptible to local events such as surface contamination, agglomeration, and composition variation, during powder manufacturing, packaging, storage, use and reuse.³

As defects arise in multiple length scales, it calls for analytical solutions with multi-length scale sampling capability. Numerous institutes have engaged in standardizing testing methods for AM powder feedstocks¹³. This white paper is not intended to repeat



Scheme 1. Illustrative PBF and DED AM processes, and the powder/beam interaction in the melt pool

these efforts; rather, we focus on selecting a few techniques, each with certain length-scale sampling capability, for identifying and quantitatively assessing the quality of AM metal powder feedstocks, e.g. Ti6Al4V AM powder (Figure 1). Combination of these techniques (Scheme 2) enable multiscale sampling and uniformity assessment of AM metal powder feedstock:

- from single particle to 10⁷⁻⁸ particles
- from a few surface atomic layers (nm-depth) to bulk (10s-µm depth)
- from elemental information to valence chemistries, and
- from %-level composition elements to sub-ppm trace impurities

2. SURFACE CHEMISTRY CHARACTERIZATION OF AM METAL POWDER FEEDSTOCK

2.1 Volume fraction of the native oxide film on AM metal powder "God made the bulk; the surface was invented by the devil – Wolfgang Pauli". AM metal powders carry 10⁴⁻⁵ - fold more surface and sub-surface atom population than typical bulk materials. These surface and sub-surface atoms are prone to reacting with residual oxygen, even at the highest practical vacuum that could be attained. For common reactive metals, such as AI and Ti, only at extremely low oxygen partial pressures, e.g., 10⁻¹⁶ atm for liquid Ti,⁴ can oxidation be avoided. Thus, AM metal or alloy powders containing reactive metals, such as AI, Ti, Cr, Zr, Nb, and Ta, are known to develop conformable, continuous, native oxide thin films. The thickness of these films can vary from a few to tens of nanometers, depending on manufacturing processes, storage conditions and thermal history.

The volume fraction of surface oxide can be estimated for particles



Figure 1. Secondary electron images of Ti6Al4V powder at 50x, 200x, 1000x, and 2500x magnifications

with perfect sphericity, if the oxide film is uniformly covering the particle, using the following equation:

Oxide Vol% =
$$[1 - (1 - 2t/d)^3] \times 100\%$$

 $\approx \frac{-6t}{d} \times 100\%$ when $\frac{t}{d} \propto 0$

where d – particle diameter, and t – oxide film thickness. It shows that the oxide volume fraction increases linearly with oxide film thickness, but inverse proportionally with the particle size. Figure 2 presents a few slices of correlation of the estimated oxide volume with oxide film thickness for spheric particles in $5-50 \mu m$ diameter range. For a particle of 10 μm in diameter, the volume fraction of the surface oxide can be up to 1.2 v% for powders developed an oxide film thickness of 20 nm, which is common for Ti6A4V AM powders produced by plasma atomization.



Scheme 2. Suggested characterization techniques for qualifications of AM metal powder feedstock. Only those in bold are demonstrated in this paper.



Figure 2. Correlation of estimated oxide volume fraction (v%) with oxide film thickness and particle diameter for spherical Ti6AI4V AM powders

This oxide film is rich in chemistry and physics, e.g., surface – OH, oxygen vacancies, cation vacancies, amorphous oxides, and dramatic impurity enrichment driven by segregation. All alter, and often, increase surface polarity and binding energy for moisture and organic contaminant physisorption. They represent a significant source for defect formation. Studying these details

requires techniques with nm-spatial resolution for elemental and chemical information.

2.2 Determination of oxide thickness and depth profiling of single AM metal particle by Auger Electron Spectroscopy (AES) The oxide film developed on metal powder can be problematic for AM processing, causing partial melting or lack of fusion, balling,



Figure 3. Secondary Electron Image (SEI) and Auger surface survey spectra on multiple AM Ti6Al4V particles (Sigma Aldrich). Probed particles are 20-30 µm in diameter. One area was analyzed per particle (circled in red). Surface Cu and C contamination was identified. Ti, O and Al are present within the top 5 nm as composition elements, but V is absent



Figure 4. Auger depth profiling on two AM Ti6Al4V particles (Sigma Aldrich), showing surface Cu and C contamination at the top 5 nm. Inserted are the SEI image and sampling locations on the particle. The two particles show significant difference in oxygen, with determined oxide thickness 8 nm (a) and 6 nm (b), respectively.

poor wetting, and evaporation loss of key alloying elements, e.g., Cr and Mo as volatile oxides when they are enriched in the surface. AES is a surface-sensitive analytical technique that utilizes a high-energy electron beam as an excitation source to probe the elemental composition of top 3 - 25 nm. With a small electron beam diameter, AES can accurately position and focus the electron beam on a small area (< 25 nm) of a particle. As such, AES is well suited to measure oxide thickness and depth profiles of compositional elements above sub-% level on individual AM metal powder particle.

Figure 3 shows the secondary electron images and AES survey data of multiple AM TiAl4V powders. Particles probed are 20-30 μ m in diameter, with one area analyzed per particle. Surface %-level Cu and C impurities were detected in the top 5 nm. Carbon is the source of carbide inclusions, while Cu can induce contamination cracking.⁵

Figure 4 presents the depth profiling of two Ti6Al4V particles in nm-resolution, showing difference in oxygen, carbon, and Cu profiles. Vanadium was absent in the top few nanometers. indicating that the top oxide layers are comprised of Ti and Al oxides only. Two particles also developed different oxide thickness, 6 and 8 nm, respectively. These results demonstrate that AES can provide atomic level details relevant to defection formation in AM parts, including surface contamination, oxide composition, element concentration gradient, and oxide thickness on single particle, at nm-spatial resolution. By surveying multiple particles, it also enables particle-to-particle consistency evaluation.

2.3 Surface contaminants and elemental mapping of multiple AM powder particles by TOF-SIMS

Time-of-Flight Secondary Ion Mass Spectrometry (TOF-SIMS) is another surface analytical technique. It is a great technique for analyzing trace and thin organic on solid surfaces. It will also detect elemental species to trace levels. Features down to a few microns in size and one nanometer thick can be analyzed.

The technique uses an ion beam and mass spectrometer to analyze the sample. An ion beam is pulsed to the sample surface causing a pulse of sample ions to be ejected. These secondary ions are accelerated in an electric field and the flight times to a detector are measured. Ion kinetic energies being equal means lighter ions will have higher velocities and will arrive at the detector first, such as hydrogen, and heavier ions will get there later such as organic molecules. Measuring flight time very accurately allows for determination of mass and molecular formula. Generated are high resolution mass spectra, images, and depth profiles.

Figure 5 presents the TOF-SIMS data of Ti6Al4V, NiTi and Al powders (Sigma Aldrich) in negative ion mode. Based on the mass fragmentation pattern, the surface contamination nature can be identified, for example,

- Ti6Al4V surface had phthalate contamination, OH and corrosive Cl, Br, Phosphate, S, and nitrogen oxide species
- NiTi surface had detergent contamination
- Al surface was decorated by various AI-OH, AI-O chemistries

Figure 6(a) presents the TOF-SIMS ion images of AM Ti6AI4V powder surface. Surface compositions were evaluated on particles



Figure 5. TOF-SIMS spectra of Ti6Al4V, NiTi and AI powders in negative ion mode.





Figure 6. (a) TOF-SIMS ion image of AM Ti6Al4V powders; (b) Surface concentration of Ti, V, Cu, and Na of particles "1" through "8", normalized to AI signal (AI = 100). Information depth is approximately 1 nm. Particle-to-particle variation are presented in the legend, as average \pm SD over eight particles.

labelled "1" through "8". The relative concentration is normalized to AI signal (AI = 100), from an estimated sampling depth of 1 nm. Figure 6(b) illustrates several species of high ion signal intensity, including Ti, V, Cu, Na, and characteristic hydrocarbon fragment $-C_3H_5$. The mean value and standard deviation were evaluated over eight particles, with Ti/AI 96±58, V/AI 8±3, Cu/AI 48±23, Na/AI 112±59, and C_3H_5 /AI 16±9. The large standard deviation indicated that particle-to-particle chemistry variation is significant, whether for composition elements (Ti and V), elemental contaminants (Cu and Na), or hydrocarbon contaminant ($-C_3H_5$).

These surface characteristics could introduce defects in finished

AM parts by various mechanisms, such as poor interlayer fusion, gas porosity (H_2O and H_2), carbide inclusions, corrosion-susceptible species (CI, Br, S, P, NOx). Surface residual moisture and -OH groups also increase the susceptibility to humidity and therefore affect the flowability of AM powder feedstock.

3.3 Surface bonding chemistry of AM powder by XPS at $10^{7\text{-}8}$ particle scale

X-Ray Photoelectron Spectroscopy (XPS Spectroscopy) uses monochromatic X-rays to irradiate a sample. The binding energies of emitted photoelectrons are characteristic of the elements present on the surface and their valence states. Since only

photoelectrons from the top 5 to 10 nm can leave the sample surface and be detected, XPS is a truly surface analysis technique. It can provide both elemental and chemical bonding information. The XPS analytical area used for this analysis is 1.5 mm x 0.6 mm, which is ten orders of magnitude greater than that of AES (< 25 nm). For AM powders, this implies that the elemental and bonding information is averaged over $10^{7.8}$ particles, instead of individual particle by AES.



Figure 7. XPS survey spectrum of Ti6AI4V AM powder

XPS is commonly used to determine quantitative atomic composition and chemistry. It can detect all elements, except for H and He. For most of elements the detection limits are from 0.1 to 0.5 at% within the top 5 nm depth (Figure 7). Table 1 demonstrates the compositional analysis of Ti6AI4V AM powder, revealing contamination by C, Cu, and several low melting point impurities such as Cu, Zn, Cd, and Ag. The low V content is also aligned with AES and TOF-SIMS findings.

Table 1. Atomic concentration (%) of Ti6Al4V AM powder as

determined b	by XPS
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Sample	С	Ν	0	AI	CI	K	Ti
Ti6Al4V AM Powder	22.8	1.1	51.9	5.0	0.3	0.03	14.7
Sample	V	Cu	Zn	Ag	Cd	W	
Ti6Al4V AM Powder	0.5	2.7	0.5	0.1	0.2	0.3	

We also acquired detailed high resolution spectra to determine bonding chemistries of the powder components (see the detailed spectra of AI and Ti in the oxide layer of the AM Ti6AI4V powder in Figure 8). The AI is found exclusively in the form of oxide, while the Ti is present in three forms: 89% Ti0₂, 5% TiN, and 6% Ti metal. Since XPS information comes from a sample depth of 5 nm, the multiple Ti chemistries detected here reveal that while the majority of powder surface (~90%) is covered with Ti0₂ oxide over 5 nm thick, a few percentages having oxide layer thickness less than 5 nm (hence the detection of Ti metal). There is also a small percentage of the powder surface covered with TiN. Such complexity in surface chemistry will no doubt add uncertainty in AM manufacturing.

3. BULK CHEMISTRY CHARACTERIZATION OF AM POWDER FEEDSTOCK

3.1 Composition and impurity analysis at 10⁵⁻⁸ - particle scale

High purity feedstocks with tight chemical composition control are the foundation for a microstructure to achieve ultimate mechanical properties. Variation in composition brings about several porosity formation risk: (1) lower eutectics broadens solidification temperature, leading to solidification cracking. An



Figure 8. XPS spectra of Ti6Al4V powder. The titanium chemistry constituting 89%TiO2, 5% TiN, and 6% Ti metal; and Al chemistry constituting 100% aluminum oxide.

alloy with a wide solidification temperature range may also exhibit a less coherent dendritic structure during solidification, thus preventing liquid from backfilling to shrinkage cracks.⁵ (2) change in density, heat capacity and thermal conductivity can lead to uneven beam energy absorption, triggering various AM process related porosity mechanisms, e.g., lack of fusion, keyhole collapse, sputtering, etc. Presence of light elements, such as C, H, O and N, can lead to gas porosity, and various precipitates and inclusions. Some impurities, even at trace levels, can have tremendous impact, often detrimental to reliability: (1) S and P are known to cause solidification cracking for ferrous and nickel alloys, as are Mg and Cu impurities to aluminum alloys.⁵; (2) Low melting point impurities (including Zn, Ga, Cd, In, Sn, Sb, Pb, and Bi), and S, Cl, As, Se, and Te, are responsible for drop in rupture toughness and corrosion resistance; and (3) leachable heavy metals from AM medical devices can generate toxicity concerns, as specified in USP < 232> and ICH Q3D, including As, Cd, Hg, and Pb.

Techniques with large sampling sizes are critical to provide complete and representative assessments of feedstock compositions. However, suitable analytical protocols must be developed and qualified to provide sensitive, precise, accurate, robust, and full survey assays. As an example, Eurofins EAG Laboratories participated in an interlaboratory analysis program organized by LGC Standards Ltd. for such development of methods. Table 2 shows our results from that interlaboratory study for IARM Ti64P-18 Additive Manufacturing Powder. We used Inductively Coupled Plasma - Optical Emission and Mass Spectrometry (ICP-OES/MS) methods and Inert Gas Fusion and Combustion techniques (IGA) for this study. These techniques require sampling amounts in the range of 0.1 g to 1 g (equivalent to about 10⁷⁻⁸ particles) for determining mass fractions of analytes listed in Table 1. The high accuracy and precision demonstrated here confirms that optimized ICP-OES/MS and IGA test methods can readily capture within lot, and lot-to-lot chemistry variations in this kind of AM powder feedstocks.

Table	2.	Test	Results	on	LGC	-	IARM	Ti64P-18	Additive
Manut	act	uring	Powder						

	EAG	Certified	
Elements	Technique	Mean ± SD (n=4), %mass	Mean ± U _{CRM} *, %mass
Ti	ICP-OES	88.9 ± 0.01	(88.7)
AI	ICP-OES	6.64 ± 0.01	6.47 ± 0.09
Fe	ICP-OES	0.209 ± 0.001	0.216 ± 0.005
V	ICP-OES	4.30 ± 0.01	4.24 ± 0.05

С	IGA	0.048 ± 0.001	0.051 ± 0.004		
	(Combustion				
	– IR)				
0	IGA (Inert	0.17 ± 0.004	0.15 ± 0.02		
	Gas Fusion				
	– IR)				
S	IGA	0.0013 ± 0.0005	0.0014 ±		
	(Combustion		0.0006		
	– IR)				
Mn	ICP-MS	0.011 ± 0.0004	0.011 ±		
			0.0002		
Р	ICP-MS	0.0010 ± 0.0004	(0.0010)		
Cu	ICP-MS	0.0062 ± 0.0004	(< 0.0050)		
* uncertainty associated with the measurement was estimated					
with cover	with coverage factor $k = 2$ at approximately 95% confidence				

Aside from solution based ICP-OES/MS, solid sampling high mass resolution glow discharge mass spectrometry (GDMS) is another suitable analytical technique for chemical analysis of AM powder feedstocks. The main advantages of GDMS as compared to other techniques are: (1) direct sampling, thus avoiding tedious sample preparations; (2) full survey elemental analysis capability, allowing determination of up to 72 elements in a single test, including all stable isotopes [6]; and (3) superior sensitivity at sub-µg/g levels, even for such critical elements as P, S, Cl, As, Se, Bi, among others.

Typically, GDMS measurements are evaluated based on atomizing several mm3 of volume fractions (8 - 10 mm in diameter x tens of µm in depth), which are equivalent to tens of mg sampling amounts, or about 105 particles per test. Hence, GDMS is well suited as a production control tool to monitor trace and ultra-trace level fluctuation of all detrimental impurities not only in feedstocks but also in final metal components that are intended to operate under harsh / extreme working environments. As an example, the smallest concentration (or amount) of analytes that are typically reported from GDMS measurements for selected impurities in Ti6AI4V AM powder sample are summarized in Table 3. Note that in titanium-based samples either an alternative discharge gas (Krypton instead or Argon) needs to be used or the glow-discharge source needs to be operated in pulsed fast-flow modes to measure mass fractions of certain elements with low specification limits, such as yttrium with max 50 µg/g per ASTM F3007.

Therefore, it is recommended that for AM metal parts graded for critical applications, such as Inconel® 718 and Haynes® 282 superalloy, their powder feedstock be evaluated with advanced GDMS methods for key impurities listed in Table 3.

level.

Table 3. GDMS analytical characteristics for selectedimpurities in Ti6Al4V AM powder

GDMS Analytical Capability		Impurity Role in Ti6Al4V					
Elemental Capability (Partial)	Reporting Limit, µg/g	Solidification Cracking	Mechanical Strength	Corrosion Resistance	Fatigue Lifetime	Toxicity	
В	0.01	—	1	—	—	—	
Si	0.1	_	↑	_	_	—	
S	0.01	Ŷ	↓	↓	Ļ	—	
Р	0.01	Ŷ	↓	\downarrow	Ļ	—	
CI	0.01	_	↓	↓	Ļ	—	
As	0.5	_	↓	↓	Ļ	1	
Se	1	↑	\downarrow	↓	Ļ	1	
Те	0.1	↑	↓	↓	Ļ	—	
Cr	0.1	_	—	_	_	1	
Fe	0.1	—	—	—		—	
Cu	0.1	Ŷ	↓	↓	Ļ	1	
Zn	0.5	—	↓	↓	Ļ	—	
Y	200*/15**	—	—	—	—	—	
Мо	0.5	_	Ŷ	↑	1	1	
Cd	0.1	_	↓	↓	Ļ	1	
In	0.01	_	↓	↓	Ļ	—	
Sn	0.1	_	↓	↓	Ļ	—	
Sb	0.5	—	↓	↓	Ļ	—	
Hg	0.1	—	↓	↓	Ļ	1	
Pb	0.05	—	↓	↓	Ļ	1	
Bi	0.05	—	\downarrow	\downarrow	Ļ	—	
* Y reporting limit using Ar as discharge gas; ** the same by fast-flow test method. \downarrow decrease; \uparrow increase; — no change or unknown							

3.2 Fractional gas analysis of O, N and H at 10⁷⁻⁸ – particle scale Taking advantage of the temperature-programming capability of specific inert gas fusion (IGA) instrument models, Eurofins EAG Laboratories also developed fractional gas analysis protocols for quantitatively assessing the O, N and H chemistries in powders, such as surface and interface oxygen, oxide precipitates, interstitial oxygen, surface -OH or physiosorbed moisture, from % levels to µg/g levels.⁷ The sampling amounts in the fractional analysis methods are the same as in standard IGA protocols, which are between 0.1 and 1.0 g per test. These amounts are equivalent to about 10⁷⁻⁸ particles per test.

Figure 9(a) illustrates the principles of the fractional gas analysis method. Figure 9(b) shows the oxygen releasing profile of Ti6Al4V AM powder acquired by fractional oxygen analysis method. In this example two distinct oxygen releasing peaks are observed, indicating there are at least two types of oxygen containing groups / species present in this specific example. Previously, AES data have revealed that at least a significant portion of oxygen in AM Ti6Al4V powder is present in the form of surface oxide film. However, as a surface technique, AES is limited to provide surface information. On the other hand, fractional O analysis, as an inert gas fusion technique, detects oxygen based on the carboreduction activity of oxygen in the sample. Surface oxygen is more reactive therefore will be released even at a temperature below fusion. This is not the case for interstitial oxygen: the latter will diffuse out the sample only in the molten state. Therefore, fractional O analysis provides a quantitative means to speciate surface and interstitial oxygen in AM powders, as demonstrated in Figure 9(b).

Notice that the ramp mode yielded about 200 μ g/g O and 20 μ g/g H lower values than the total O and H determined by the flash mode (Table 4). This difference, with mass ratio O/H ~ 10/1, is attributed to moisture and surface residual -OH groups in Ti6Al4V powder,

Figure 9. (a) Fractional IGA O, N and H analysis method development protocol, with N as example; and (b) oxygen releasing profile of Ti6Al4V AM powder acquired by fractional IGA technique, with two distinct oxygen releasing peaks observed.

which are not detected in fractional analysis mode. Previously, TOF-SIMS analysis has identified moisture and -OH groups on Ti6Al4V powder surface. Thermal Desorption Spectroscopy (TDS) can provide more detailed moisture desorption behavior. However, quantification is challenging.^[8] Herein, fractional gas analysis methods not only enable speciating various O, N and H bonding chemistries, but also provide a quantitative means to assess sub-% to μ g/g level moisture and surface -OH groups in gram-level sampling. This information could be key for gas porosity control (such as H₂O, H₂), as well as for powder agglomeration and flowability control.

Analysis Mode	0(n=3), μg/g	H(n=3), μg/g	Remark
Flash Mode	1340 ± 70	30 ± 1	ASTM E1409 method
Ramp Mode	1140 ± 70	10 ± 3	EAG fractional analysis protocol
Moisture/ Residual surface -OH (by Difference)	200	20	In consistent with primary loss of H_2O based on O/H ratio 10/1 (mass/mass)

Table 4. Fractional O and H analysis of Ti6Al4V AM powder

SUMMARY

Satisfactory grade metal powders for AM should possess the following characteristics: high chemical purity and uniformity in allotropic form (no density changes), thermal conductivity, solubility of all critical elements, and spherical shape with desired particle size distributions. In this white paper, we identified and quantitatively assessed the chemistry of AM feedstock that is fundametal to the above requirement using Eurofins EAG Laboratories's variuos bulk and surface characterization tools. Surface techniques provide fine structural details with atomic and molecular information, at nm – spatial resolution, from single particle to mutiple particles; and bulk techniques provide a macrocale, quantiative assessment of composition consistency and purity level. Table 5 provides a summary of the technique features, sampling length scale, and relevant analytical information.

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Table 5 Multiscale assessment of AM metal powder feedstocks – techniques, sampling scale and analytical information

Tecl	nnique	Sampling Scale	Analytical Information
	ICP-OES	• 0.5 – 1.0 g	 accurate alloy composition analysis from % to sub%
SIS		• 10 ⁶ – 10 ⁷ particles	measurement uncertainty less than 1%rel in high performance mode
laly	IGA	• 0.1 – 1.0 g	• accurate determination of trace gas-forming element content C, H, O, N and
k Ar		• 10 ⁶ – 10 ⁷ particles	S down to ppm level
Bul	ICP-MS	• 0.1 – 1.0 g	• accurate trace metal/metalloid impurity analysis with detection limits generally
ale		• 10 ⁶ – 10 ⁷ particles	in ppm level
OSC			excluding halogen
laci	GDMS	• 10s mg	• Survey trace metal/metalloid/nonmetal impurity analysis with detection limits
2		 10⁵ particles 	generally at sub-ppm level
			Including S and halogen
	TOF-SIMS	 Analytical area: 250 μm x 250 μm 	 information depth: a few surface atomic layers
lysis		• 10s-100s particles	 Survey identification of molecular contaminants physisorped on the surface, particularly of organic nature
Ana			 surface composition uniformity from particle to particle
ace	AES	• Analytical area: < 25 nm	Information depth 5 nm or less
urfa		Single particle	Single particle composition down to sub-% level
le S		 Sampling depth: 1-10 nm 	 Oxide thickness evaluation with nm- spatial resolution
sca			Composition gradient within single particle
cro-	XPS	• Analytical area: 1.5 mm x 0.6 mm	Information depth 10 nm or less
Mi		• 10 ⁷⁻⁸ particles	Surface composition above sub-% level
anc			Surface bonding chemistry
cro-			Surface contaminants
Mag	Fractional	• 0.1 – 1.0 g	• O, N and H chemistry speciation (e.g., surface vs bulk) down to ppm level
	IGA	• 10 ⁶ – 10 ⁷ particles	 Quantitation of trace moisture and surface residual -OH polar group down to ppm level

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